

RESEARCH

Influence of the physiological medium on the mechanical properties of bone cement: Can current studies be extrapolated? ☆, ☆ ☆

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KEYWORDS

Polymethylmethacrylate;
Bone cement;
Antibiotic loaded cement;
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Abstract

Purpose: The use of bone cement is widespread in orthopedic surgery. Most of the mechanical tests are performed in dry medium, making it difficult to extrapolate the results. The objective of this study is to assess if the mechanical properties of polymethylmethacrylate (PMMA), obtained in previous reports, are still present in a liquid medium.

Materials and methods: An experimental study was designed with antibiotic (vancomycin) loaded PMMA. Four groups were defined according to the medium (dry or liquid) and the pre-conditioning in liquid medium (one week or one month). Wear and flexural strength tests were performed according to ASTM and ISO standards. Volumetric wear, friction coefficient, tensile strength, and Young's modulus were analyzed. All samples were examined by scanning electron microscopy.

Results: The samples tested in liquid medium showed lower wear and flexural strength values ($P < .05$). The kind of wear was modified from abrasive to adhesive in those samples studied in liquid medium. The samples with a pre-conditioning time showed lower values of wear ($P < .05$).

Conclusions: Caution is recommended when extrapolating the results of previous PMMA results. The different mechanical strength of the cement in a liquid medium, observed in saline medium, is much closer to the clinical situation.

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PALABRAS CLAVE

Polimetilmetacrilato;
Cemento óseo;
Cemento con
antibiótico;
Infección protésica

Influencia del medio fisiológico sobre las propiedades mecánicas del cemento óseo. ¿Son los estudios actuales extrapolables?

Resumen

Objetivo: El uso del cemento óseo está muy extendido en COT, existiendo multitud de estudios experimentales que lo avalan. La mayoría de los ensayos mecánicos están realizados en seco, lo que cuestiona la extrapolación de los resultados a la clínica. El objetivo de este estudio es evaluar si las propiedades mecánicas del polimetilmetacrilato (PMMA) obtenidas en series previas en seco, se mantienen en un medio fisiológico.

Material y método: Se ha diseñado un estudio experimental para evaluar este aspecto, utilizando PMMA con antibiótico (vancomicina). Cuatro grupos fueron definidos en función del medio estudiado (seco o líquido) y de la realización de un acondicionamiento previo en suero fisiológico (una semana o un mes). Se hicieron estudios de desgaste y resistencia a flexión según las normativas ISO y ASTM, valorando el desgaste, el coeficiente de fricción, la resistencia a la rotura y el módulo de Young. Las muestras fueron analizadas mediante microscopía electrónica.

Resultados: Las muestras ensayadas en medio líquido presentaron menores valores de desgaste, así como menor resistencia a flexión, obteniéndose significación en el desgaste. El tipo de desgaste se modificó de un desgaste abrasivo a uno adhesivo en aquellas muestras estudiadas en medio líquido. El tiempo de acondicionamiento proporcionó menores valores de desgaste ($P < 0,05$).

Conclusiones: Se recomienda precaución a la hora de extrapolar los resultados de los estudios sobre PMMA en seco dado el diferente comportamiento mecánico del cemento en un medio líquido mucho más cercano a la situación clínica real, como es el suero fisiológico.

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Introduction

Since the use of polymethylmethacrylate (PMMA) by Dr. Charnley in the 1960s as a method of fixation for hip arthroplasties,^{1,2} PMMA has been shown to be one of the best methods of implant fixation in orthopedic surgery, with survival rates of more than 90% at 15 years in knee⁴ and hip³ arthroplasties. In addition to its usefulness in fixation, PMMA has been shown to be the best vehicle to date for using high amounts of antibiotics in the treatment of osteoarticular infection (and especially in prosthetic infection), achieving high local concentrations with very few systemic effects. This is particularly important, given that an increase of nearly 50% in the rate of prosthesis revision caused by infection is projected by 2030.⁵

The usefulness of PMMA as a method of fixation, as well as growing interest in its use in the treatment and prophylaxis of prosthetic infection, has made it into one of the most frequently studied materials in our environment; this in turn has led to the appearance of multiple commercial preparations and the publication of minimum requirements by international agencies such as the ISO and the ASTM.⁶⁻⁸ Given that the great majority of studies performed to date have been under experimental conditions of dry medium, it is difficult to extrapolate these results correctly to clinical practice. This difficulty undoubtedly is of special interest when studying PMMA used with antibiotics, whose elution in liquid medium inevitably affects the mechanical characteristics of PMMA.

The objective of this study was to assess the influence of a liquid medium such as saline solution on the resistance and wear of bone cement mixed with an antibiotic, and whether such influence varied over time.

Materials and methods

We performed an experimental study to assess the effect on liquid medium on bone cement. The PMMA used was bone cement that was quick setting, of high viscosity and preloaded with 0.5 g of gentamicin Palacos® R+G (Heraeus Medical GmbH, Wehrheim, Germany), because of its wide use and its good survival data in various series.^{9,10} To each commercial preparation of cement, we added a vial of 1 g of powdered vancomycin (Normon EFG, Tres Cantos, Madrid, Spain) manually to reproduce the treatment conditions of an infected arthroplasty.

Two types of samples were prepared: circular and rectangular. Before sample preparation the cement had been stored at controlled temperature and relative humidity. The components were not cooled beforehand; they were mixed in a tray manually. We added vancomycin independently, following the method of Frommelt and Kühn¹¹ for manual addition of antibiotics, previously adding the same amount of powdered antibiotic as of polymer in a tray for a minute until we achieved a homogeneous mixture of the powder. Room temperature at the time of mixing was 23 °C, with a relative humidity of 55–60%. The mixing process was carried out following the recommendation of the manufacturer and ASTM F451-99⁶ and ISO 5833:2002⁸ regulations. Each 20-ml vial of monomer was mixed with a 40-g sachet of polymer, added in that order in a reusable plastic tray. The mixture was prepared by stirring in a clockwise direction in homogeneous frequency for a timed period of 30 s. Once the paste was achieved, it was left to set until it was shown that the mixture would not stick (2 min at work temperature), then beginning the preparation of the samples.

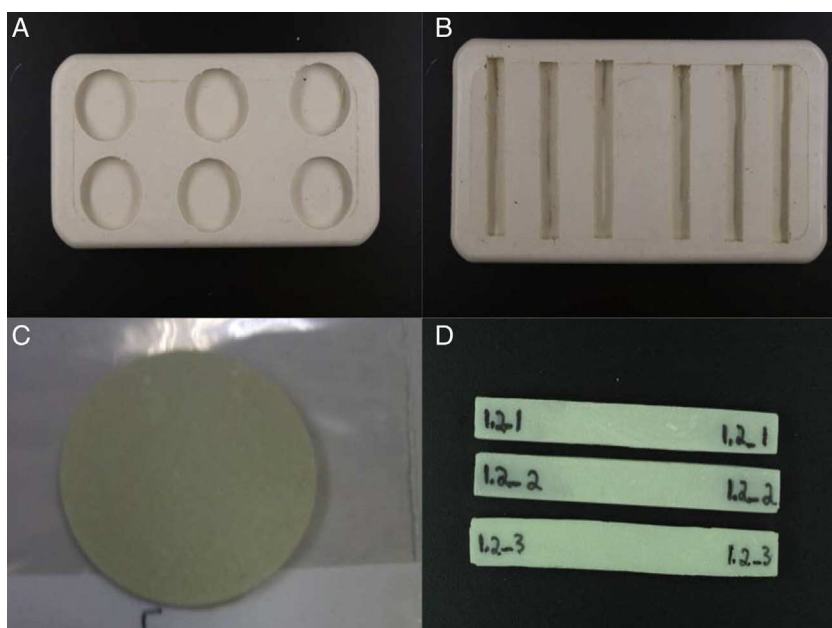


Figure 1 Molds used to prepare the samples of wear (A) and flexion (B). Samples before their testing, once removed from the mold (C and D).

To prepare the samples we used a predesigned mold made of silicone (Fig. 1A and B), with circular samples 30mm in diameter and 4mm thick (Fig. 1C) and rectangular samples 79mm long, 10mm wide and 4.5mm high (Fig. 1D). The process of preparing these was similar, using cement in ductile phase to fill the molds, leaving them to set under a continuous weight of 10kg to become compact and to obtain homogeneous samples. Following a hardening period (10–12 min) we removed the samples from the molds. Each bag of cement yielded enough for the preparation of 6 samples in 1 of the molds. The circular samples were used to study wear, while the rectangular ones were used to study resistance to fracture.

We defined various groups based on the conditioning process to which they were submitted, yielding 4 groups for the circular samples and 2 groups for the rectangular samples (Table 1). The conditioning process consisted of immersing the samples in isotonic saline solution (B. Braun, Melsungen, Germany) during the appropriate time for each group, maintaining the samples at a constant temperature of 37°C by incubation with a heater. These conditions attempted to replicate a medium similar to that which exists in a joint. Three homogeneous samples were prepared for each study group.

For the determination of wear and of the coefficient of friction, we performed mechanical testing following Standard ASTM G99-05.⁷ For the production of a wear track, we used a PIN-ON-DISK tribometer (Microtest, Madrid, Spain), with a 304 stainless steel ball 6 mm in diameter. The test conditions used were with a normal load applied of 15 N, a described path of 1000 m, and a frequency of 120 rpm (Fig. 2B and D). For the tests performed with the samples submerged in saline solution, a recipient was attached to the tribometer plate, where the samples covered in saline solution were introduced. The measurement of the wear track

and its width was done with a v-20A Nikon Profile Projector (Nikon instrument INT, NY, USA). The use of a trigonometric model let us measure the wear obtained, defining the volume lost in mm³/Nm (Fig. 3). All of the samples tested were observed using a scanning electron microscope, with a previous requisite gold dust coated by sputtering.

To assess the resistance of the samples at a moment of flexion, we carried out testing using the international standard ISO 178:1993 and its Spanish modification UNE-EN-ISO 178. We used a universal testing machine (IB-MU4, IBERTEST, Ibertest group, Madrid, Spain) with 3-point flexion testing jaws, placing each sample over the lower points and applying a central force over the upper face of the sample. The distance between both lower supports was 64 mm,

Table 1 Definition of the 4 groups based on conditioning process.

	Circular samples	Rectangular samples
Group 1	No conditioning. Samples tested in dry medium	No conditioning. Samples tested in dry medium
Group 2	Samples tested in liquid medium without prior conditioning	–
Group 3	Samples tested in liquid medium after a week of conditioning	–
Group 4	Samples tested in liquid medium after a month of conditioning	Samples tested in liquid medium after a month of conditioning

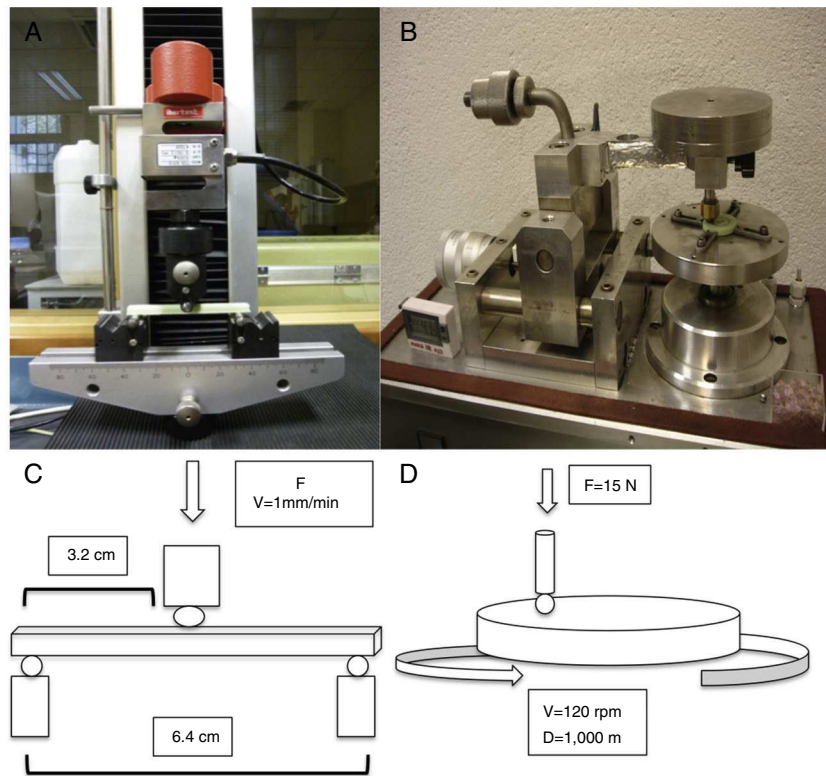


Figure 2 Instruments used to carry out the testing and the conditions applied. Universal testing machine (A) and tribometer (B). Illustration of the study conditions for flexion (C) and wear (D) testing.

applying the force in the central point at a speed of 1 mm/min (Fig. 2A and C).

For the statistical analysis, we used the SPSS® version 15.0 computer package for MS-Windows (SPSS Inc., Chicago, USA). The ANOVA test was used for the comparison of the

variables studied among the various groups for the wear tests, and Student's *t*-test for independent samples in the mechanical resistance studies. Statistically significant differences were defined as those having *P* values lower than 5% ($P < .05$).

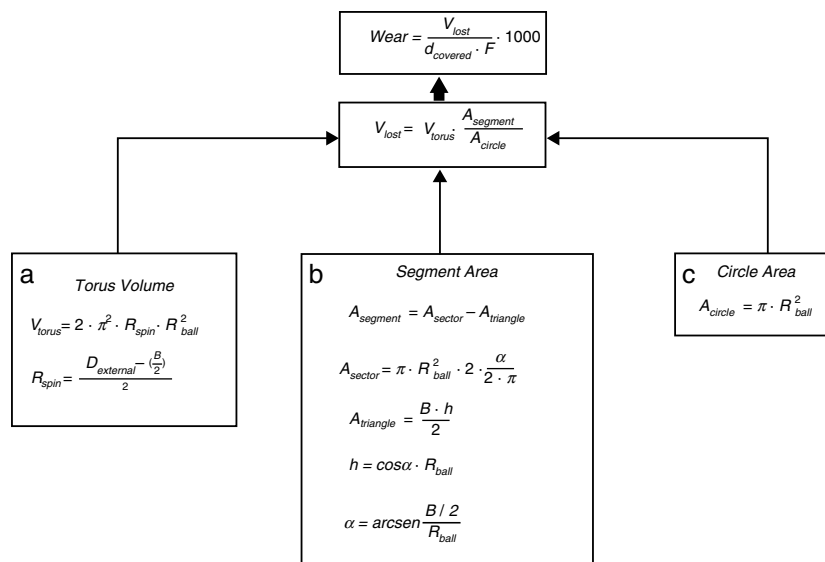


Figure 3 Trigonometric model used to calculate wear; *d* (distance covered = 1000m), *F* (force applied = 15N), V_{lost} (volume lost due to wear), V_{torus} (volume of the rotation torus), R_{spin} (radius of the wear track), R_{ball} (radius of the wear ball = 6 mm), D_{external} (external diameter of the wear track), *B* (width of the track), *A* (area), and *h* (height).

Table 2 Mean results and standard deviation obtained in wear testing.

	Group 1 Dry medium without conditioning	Group 2 Liquid medium without conditioning	Group 3 Liquid medium 1 week of conditioning	Group 4 Liquid medium 1 month of conditioning
Wear track width	1.20 ± 0.02 mm	0.86 ± 0.01 mm	0.83 ± 0.02 mm	0.73 ± 0.01 mm
Wear track diameter	17.59 ± 0.8 mm	17.94 ± 0.9 mm	18.82 ± 0.1 mm	18.70 ± 0.1 mm
Wear	0.09 ± 0.09 mm ³ /Nm × 10 ⁻⁴	0.03 ± 0.003 mm ³ /Nm × 10 ⁻⁴	0.03 ± 0.003 mm ³ /Nm × 10 ⁻⁴	0.02 ± 0.001 mm ³ /Nm × 10 ⁻⁴
Coefficient of friction	0.72 ± 0.07	0.49 ± 0.08	0.44 ± 0.05	0.36 ± 0.08

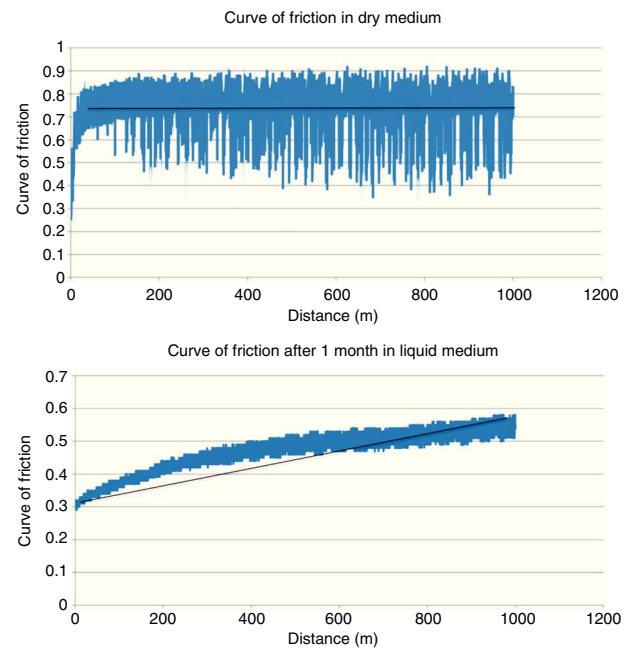


Figure 4 Evolution of the coefficient of friction in liquid medium (upper figure) and in dry medium (lower figure).

Results

Table 2 shows the results obtained in the wear testing. In the samples tested in dry medium there were wear and coefficient of friction values significantly greater than those tested in liquid medium, whatever the process of conditioning ($P < .05$). The medium of study also conditioned how wear was produced, in that continuous wear was observed in the samples in comparison to exponential wear in samples studied in liquid medium (Fig. 4). The decrease in wear observed was more than 60% (Table 2). The performance of a previous process of conditioning (Groups 3–4) diminished both wear and the coefficient of friction obtained in comparison to the samples that presented a lack of conditioning (Group 2), although there was no statistically significant difference. Increasing the time of conditioning from 1 week (Group 3) to 1 month (Group 4) produced a significantly greater decrease in the values of wear and coefficient of friction ($P = .04$).

Scanning electron microscopy (SEM) showed a smaller size of the wear tracks tested in dry medium. The wear was of the abrasive type, changing to mainly adhesive when testing the samples in liquid medium (Fig. 5).

The results obtained in the flexion testing are summarized in Table 3. Samples tested in liquid medium presented lower resistance to breaking, bearing forces of lesser magnitude and suffering deformation to a lesser degree, than the samples studied in dry medium. The stress registered in the samples studied in liquid medium was also lower than that obtained in dry medium. No variations in the model of elasticity were observed.

Discussion

The results of our study were influenced by the choices of bone cement, environmental conditions, and antibiotic.

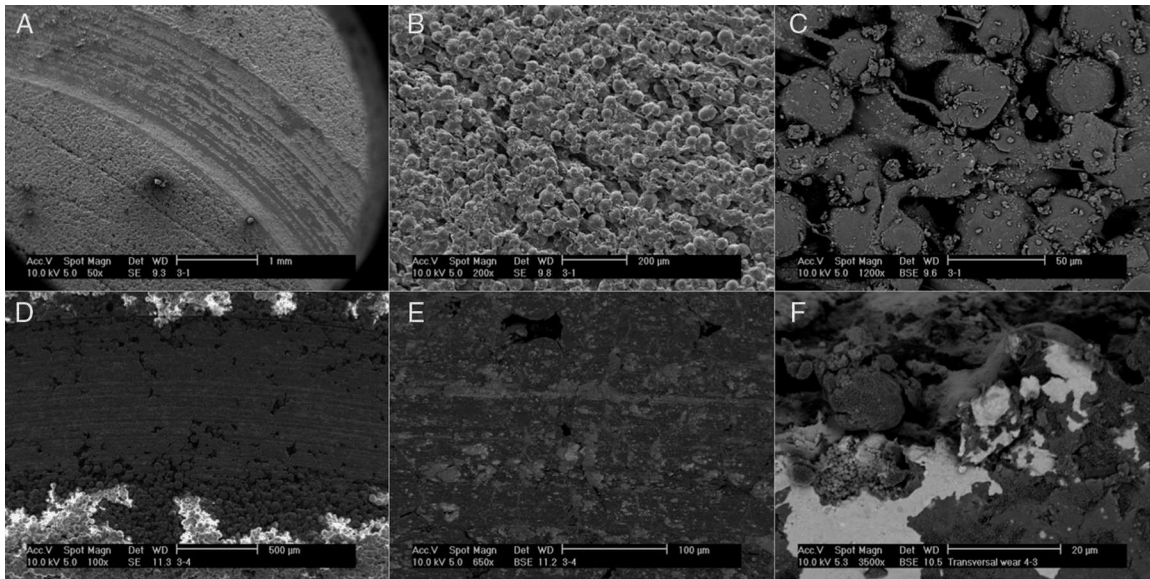


Figure 5 Images of the wear tracks obtained by electron microscope. In the upper images (A–C) abrasive wear can be seen in contrast to that obtained in the lower images (D–F). Note the particles adhered to the surface in E and (in a larger scale) in Image F.

For this study we used Palacos® R+G (Heraeus Medical GmbH, Wehrheim, Germany) as it is one of the most widely used commercial cements that had the best long-term results.^{12,13} The environmental conditions selected were defined attempting to imitate the normal conditions existing in operating rooms where bone cement is used.^{14,15} The industrial addition of a small amount of an antibiotic like gentamicin has not been shown to affect the mechanical properties in previous studies.¹⁶ The choice of vancomycin as the antibiotic was based on its wide distribution, its use as treatment of prosthesis infection associated to PMMA, and its reduced price.^{9,17} All samples were mixed manually. This method increases porosity in PMMA, which leads to reducing the mechanical resistance and increasing the elution of PMMA.^{3,18–20} This has been called into question by McLaren et al.²¹

The effect of immersing PMMA in a liquid medium has been studied previously. Schmitt et al. described an increase in cement mass when it was submerged in saline solution.²² Other authors observed a decrease in the model of elasticity as water was absorbed,²³ with PMMA even becoming saturated at 3 months without any observable changes in its properties although the water acted as an initiator of fractures.²⁴ The plasticizing effect of the water and its influence on the mechanical properties of the bone cement have been described in detail,^{22,24,25} with it being due to the

absorption of water by the PMMA, a process described in other polymers,²⁶ being cyclic.

In our study we did not find statistical significance in the changes observed in the mechanical properties of PMMA studied in dry medium as compared to that studied in liquid medium. However, there was a clear tendency to a decrease in these properties when we introduced the PMMA in a medium with liquid. These results are the same as those found in the literature. Nottrott²⁷ studied the behavior of Palacos® R+G and CMW 3 Genta® stored for 5 years in a dry medium against for 3 weeks in a medium with water; they found an increase in resistance to stress and in the model of elasticity in the samples that had been stored dry.

The wear observed in our study was low compared to the coefficients of friction obtained, with significantly lower wear in the samples studied in liquid medium. This could be due to the lubricating effect of water, the modification of the wear pattern from an abrasive behavior to an adhesive one, and to the deposit itself of substances in the wear track of the samples tested in liquid (Fig. 5A–F), although the authors have no knowledge of any prior descriptions of this phenomenon.

Bone cement is not a static component; its mechanical properties vary over time. Cizmecioglu et al.²⁸ described the influence of PMMA “aging” on its elasticity, determined by the amount of residual monomer, which has a damaging

Table 3 Mean results and standard deviation obtained in flexion testing.

	Dry medium (no conditioning)	Liquid medium (1 month of conditioning)
Max. force	0.09 ± 0.01 kN	0.06 ± 0.045 kN
Max. stress	46.3 ± 2.3 MPa	42.5 ± 2.7 MPa
Max. deformation	0.04 ± 0.02 mm	0.03 ± 0.005 mm
Young model	1814.9 ± 71.3	1819.7 ± 64.5

effect on PMMA resistance.²⁹ In our study, we obtained less wear in the samples that had undergone a process of conditioning, observing an influence of period of adaptation in this decrease; the samples submitted to a month of conditioning presented significantly less wear than the samples submitted to a week. To the best of our knowledge, there is no previous study that evaluates the time of aging in a liquid medium on PMMA resistance to wear.

In contrast to previous studies in the literature, in our study we used PMMA wear as another variable to measure the influence of the liquid medium on mechanical properties. An increase in wear could be prejudicial to implant fixation; Saleh et al.³⁰ and Goodman³¹ described how the particles of bone cement wear could be involved in periprosthetic osteolysis, although excessive wear could be useful in other situations because of the increase in elution of antibiotic present on the surface of articulating spacers. This study is an initial step in attempting to understand what happens on the surface of these spacers.

In our study we wanted to imitate the environmental conditions in a joint. To this end, we used a medium of study with saline solution, but we must accept certain limitations. A healthy joint contains, in addition to synovial liquid, various substances such as proteins, cells, glucose and so on that give it different rheological properties from those of saline solution. Using a watertight medium for producing the conditioning and wear also differs from the normal behavior of a joint, where there is a flux between absorption/production, in addition to movement, which can have an effect on the particles of wear being deposited on the cement itself and can consequently change the wear values obtained. We feel that it is important to keep these considerations in mind when interpreting the results. We do not believe that the limited number of samples represents a limitation for the results of this study, although it could indeed have limited the obtaining of statistical significance in specific groups. Other publication of special relevance in biomaterials have used similar sample sizes; examples are Unemori et al.²⁵ who utilized 3 samples to observe the absorption of water in modified PMMA, and Bridgens et al.³² who used 2 samples to study the elution and mechanical resistance of various cements mixed with PMMA.

In conclusion, the results obtained in this study show the damaging effect of the liquid medium on PMMA, which brings into question the use of the data obtained in previous studies carried out in dry medium extrapolated to clinical practice. Nevertheless, further studies that back this up are required, as well as additional studies to evaluate if the decrease in PMMA resistance and wear with vancomycin observed in this study continues in other PMMA isolated or in combination with other antibiotics.

Level of evidence

Level of evidence 1.

Ethical responsibilities

Protection of persons and animals. The authors declare that no experiments on human beings or animals were performed for this research.

Data confidentiality. The authors declare that no patient data appear in this article.

Right to privacy and informed consent. The authors declare that no patient data appear in this article.

Conflicts of interest

The authors have no conflicts of interest to declare.

References

1. Charnley J. Arthroplasty of the hip. A new operation. *Lancet*. 1961;1:1129–32.
2. Charnley J. Anchorage of the femoral head prosthesis to the shaft of the femur. *J Bone Joint Surg Br*. 1960;42B:28–30.
3. Jaeblo T. Polymethylmethacrylate: properties and contemporary uses in orthopaedics. *J Am Acad Orthop Surg*. 2010;18:297–305.
4. Rand JA, Trousdale RT, Ilstrup DM, Harmsen WS. Factors affecting the durability of primary total knee prostheses. *J Bone Joint Surg Am*. 2003;85A:259–65.
5. Kurtz SM, Ong KL, Schmier J, Mowat F, Saleh K, Dybvik E, et al. Future clinical and economic impact of revision total hip and knee arthroplasty. *J Bone Joint Surg Am*. 2007;89 Suppl. 3:S144–51.
6. American Society for Testing and Materials (ASTM) Standard 451-99a. Standard specification for acrylic bone cement. Annual book of ASTM standards, vol. 13.01. West Conshohocken, PA, USA: ASTM International; 2007.
7. American Society for Testing and Materials (ASTM) Standard G 99-05. Standard test method for wear testing with a pin-on-disk apparatus, vol. 03.02. West Conshohocken, PA, USA: ASTM International; 2010.
8. International Standards Organization (ISO). ISO 5833: implants for surgery-acrylic resin cements. Annex F. Method for determination of bending modulus and strength of cement. Switzerland: ISO Geneva; 2002.
9. Hanssen AD, Spangehl MJ. Practical applications of antibiotic-loaded bone cement for treatment of infected joint replacements. *Clin Orthop Relat Res*. 2004;79–85.
10. Penner MJ, Masri BA, Duncan CP. Elution characteristics of vancomycin and tobramycin combined in acrylic bone-cement. *J Arthroplasty*. 1996;11:939–44.
11. Frommelt L, Kühn K-D. Properties of bone cement: antibiotic-loaded cement. In: Breusch S, Malchau H, editors. *The well-cemented total hip arthroplasty*. Berlin Heidelberg: Springer-Verlag; 2005. p. 86–92.
12. De Santis R, Mollica F, Ambrosio L, Nicolais L, Ronca D. Dynamic mechanical behavior of PMMA based bone cements in wet environment. *J Mater Sci Mater Med*. 2003;14:583–94.
13. Webb JC, Spencer RF. The role of polymethylmethacrylate bone cement in modern orthopaedic surgery. *J Bone Joint Surg Br*. 2007;89B:851–7.
14. Carlsson AS, Nilsson JA, Blomgren G, Josefsson G, Lindberg LT, Önerfält R. Low- vs high-viscosity cement in hip arthroplasty. No radiographic difference in 226 arthrosis cases followed for 5 years. *Acta Orthop Scand*. 1993;64:257–62.
15. Smeds S, Goertzen D, Ivarsson I. Influence of temperature and vacuum mixing on bone cement properties. *Clin Orthop Relat Res*. 1997;334:326–34.
16. Espehaug B, Engesaeter LB, Vollset SE, Havelin LI, Langeland N. Antibiotic prophylaxis in total hip arthroplasty. Review of 10,905 primary cemented total hip replacements reported to

- the Norwegian arthroplasty register, 1987 to 1995. *J Bone Joint Surg Br.* 1997;79B:590–5.
17. Jiranek WA, Hanssen AD, Greenwald AS. Antibiotic-loaded bone cement for infection prophylaxis in total joint replacement. *J Bone Joint Surg Am.* 2006;88:2487–500.
 18. Lewis G, Janna S, Bhattaram A. Influence of the method of blending an antibiotic powder with an acrylic bone cement powder on physical, mechanical, and thermal properties of the cured cement. *Biomaterials.* 2005;26:4317–25.
 19. Messick KJ, Miller MA, Damron LA, Race A, Clarke MT, Mann KA. Vacuum-mixing cement does not decrease overall porosity in cemented femoral stems: an in vitro laboratory investigation. *J Bone Joint Surg Br.* 2007;89:1115–21.
 20. Meyer J, Piller G, Spiegel CA, Hetzel S, Squire M. Vacuum-mixing significantly changes antibiotic elution characteristics of commercially available antibiotic-impregnated bone cements. *J Bone Joint Surg Am.* 2011;93:2049–56.
 21. McLaren AC, Nugent M, Economopoulos K, Kaul H, Vernon BL, McLemore R. Hand-mixed and premixed antibiotic-loaded bone cement have similar homogeneity. *Clin Orthop Relat Res.* 2009;467:1693–8.
 22. Schmitt S, Krzypow DJ, Rimnac CM. The effect of moisture absorption on the fatigue crack propagation resistance of acrylic bone cement. *Biomed Technol (Berl).* 2004;49:61–5.
 23. Ishiyama CHY. Effects of humidity on Young's modulus in poly(methyl methacrylate). *J Polym Sci B: Polym Phys.* 2002;40:460–5.
 24. Akashi A, Matsuya Y, Unemori M, Akamine A. The relationship between water absorption characteristics and the mechanical strength of resin-modified glass-ionomer cements in long-term water storage. *Biomaterials.* 1999;20:1573–8.
 25. Unemori M, Matsuya Y, Matsuya S, Akashi A, Akamine A. Water absorption of poly(methyl methacrylate) containing 4-methacryloxyethyl trimellitic anhydride. *Biomaterials.* 2003;24:1381–7.
 26. Abenojar J, Martínez M, Velasco F, del Real JC. Effect of moisture and temperature on the mechanical properties of an epoxy reinforced with boron carbide. *J Adhes Sci Technol.* 2011;24:2445–60.
 27. Nottrott M. Acrylic bone cements: influence of time and environment on physical properties. *Acta Orthop Suppl.* 2010;81:1–27.
 28. Cizmecioglu M, Fedors RF, Hong SD, Moacanin J. Effect of physical aging on stress relaxation of poly(methyl methacrylate). *Polym Eng Sci.* 1981;21:940–2.
 29. Vallo CI, Abraham GA, Cuadrado TR, San Roman J. Influence of cross-linked PMMA beads on the mechanical behavior of self-curing acrylic cements. *J Biomed Mater Res B: Appl Biomater.* 2004;70:407–16.
 30. Saleh KJ, Thongtrangan I, Schwarz EM. Osteolysis: medical and surgical approaches. *Clin Orthop Relat Res.* 2004: 138–47.
 31. Goodman S. Wear particulate and osteolysis. *Orthop Clin N Am.* 2005;36:41–8.
 32. Bridgens J, Davies S, Tilley L, Norman P, Stockley I. Orthopaedic bone cement: do we know what we are using. *J Bone Joint Surg Br.* 2008;90:643–7.